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SOLAR/2018-79/03

Monthly Performance Report

REEDY CREEK UTILITIES

MARCH 1979





U.S. Department of Energy

National Solar Heating and Cooling Demonstration Program

National Solar Data Program

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MONTHLY PERFORMANCE REPORT REEDY CREEK UTILITIES MARCH 1979

SYSTEM DESCRIPTION

The Reedy Creek site is a two story, 5,625 square foot concrete block office building located in Lake Buena Vista, Florida. The solar energy system is designed to provide space heating, domestic hot water and space cooling.

The collector subsystem is composed of a horizontal array of 16 parabolic trough collectors, manufactured by AAI Corporation, with tracking absorber tubes. The collector array is an integral part of the building's roof, with the reflector troughs oriented so that each major axis is in an east-west direction. The 16 absorber tubes are moved in unison in a north-south direction by the solar tracking system. The total collector aperture area is 3,840 square feet. Water is used as the heat collection, transfer, and storage medium. Collected solar energy is stored in a 10,000-gallon hot water tank, located adjacent to the building and shaded by the roof. Domestic hot water is provided by a heat exchanger immersed in this tank. Space heating is provided by circulation of hot water from the storage tank through heat exchangers located in the central air distribution system. No auxiliary energy is provided for either domestic hot water or space heating.

A 25-ton absorption chiller utilizes hot water from solar storage to provide chilled water to a 10,000-gallon cold water storage tank. For space cooling, water from this cold tank is circulated through heat exchangers located in the building's central air distribution system. Auxiliary cooling is provided by supplemental cold water from the utility district's central chiller plant, which is powered by fossil fuels.

The system, shown schematically in Figure 1, has five modes of solar operation.

Mode 1 - Collector-to-Storage: This mode is entered when the collector absorber plate temperature is 10°F higher than the temperature at the bottom of the hot storage tank (water solar thermal storage). Water is circulated through the collector array-storage loop by pump Pl until the temperature of the water at the bottom of storage rises to within 3°F of that of the collector absorber plate.

Mode 2 - Storage-to-Space Heating: This mode is entered when the temperature falls below the setting of the thermostats located in the occupied areas. Since this is the only means of space heating available, no minimum tank temperature is specified. Pump P2 causes hot water to flow directly from the storage tank to the heat exchanger in the air-handling unit, and back to the storage tank.

Mode 3 - Domestic Hot Water Heating: Domestic hot water (DHW) is provided by passing city supply water through a heat exchanger immersed in the solar thermal storage tank. No conventional water heater exists, thus water is heated only upon demand. A tempering valve is used when necessary to reduce the temperature of water leaving the heat exchanger. If the water is too hot, cold supply water is mixed with it in the tempering valve before going to the domestic hot water line.

Mode 4 - Chilled Water Production: This mode is entered when the temperature of the water in the top of the solar thermal storage tank is at or above the generator operating temperature (nominally 180°F) and that of the water at the bottom of the 10,000-gallon chilled water storage is greater than 45°F. Hot water is drawn from the solar thermal storage tank to operate the generator section of the absorption chiller and cold water is circulated through the chiller from the chilled water storage. Energy is removed from the cold water, lowering its temperature; the energy is rejected though the cooling tower, and the cold water returns to the chilled water storage tank. Whenever the temperature

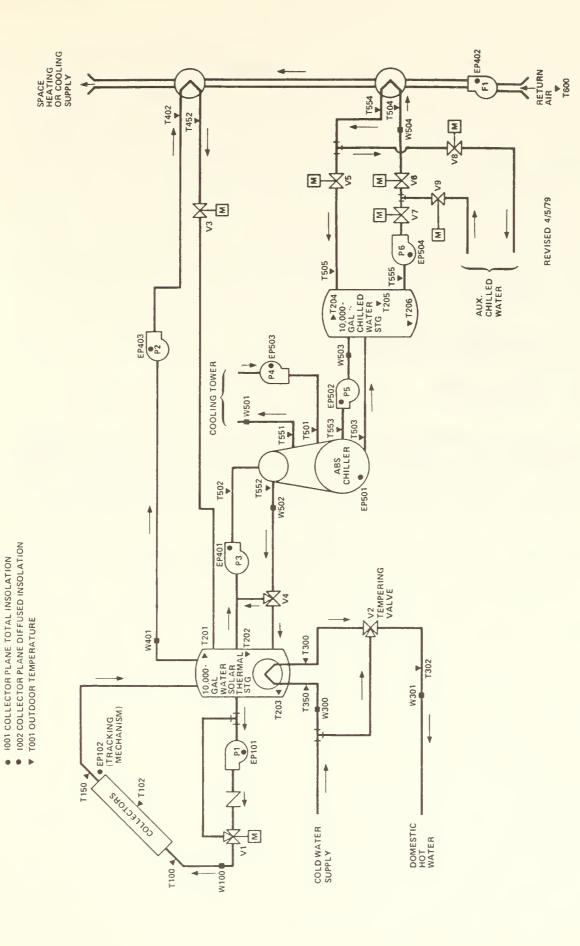


Figure 1. REEDY CREEK SOLAR ENERGY SYSTEM SCHEMATIC

of the water going to the generator exceeds the upper limit of 195°F, the water is tempered with cooler water returning through valve V4.

Mode 5 - Space Cooling: The space cooling mode is initiated when the building temperature exceeds the setting of the conditioned space thermostat. Chilled water from the chilled water storage is then circulated by pump P6 to the heat exchangers in the building air distribution system. If the chilled water storage system is not able to meet the cooling load, an auxiliary chilled water supply is available from the central energy plant.

II. PERFORMANCE EVALUATION

A. Introduction

The system performance evaluations discussed in this section are based primarily on the analysis of the data presented in the attached computer-generated monthly report. This attached report consists of daily site thermal and energy values for each subsystem, plus environmental data.

The Reedy Creek solar energy system operated continuously throughout the month of March. The domestic hot water demand was 0.17 million Btu; the space heating demand was 5.59 million Btu; the space cooling demand was 6.17 million Btu. The solar energy system supplied 100 percent of the domestic hot water and space heating requirements, and 98 percent of the space cooling requirements - these quantities are reported in the attached computer printout as loads.

B. Weather

For March, the average outside ambient temperature measured at the site was $66^{\circ}F$. The long-term average temperature is $65.9^{\circ}F$ at the Orlando weather station. The average measured insolation in the plane of the array was only 1,501 Btu/ft²-day. This is considerably less than the long-term average of 1,746 Btu/ft²-day for March, which was derived from measurements taken at the Tampa weather station.

C. System Thermal Performance

<u>Collector</u> - Of the 178.7 million Btu incident on the collector array, 29.6 million Btu were collected and delivered to the solar thermal storage tank. This represents an array efficiency of 16.6 percent. Operating energy of 1.6 million Btu (463 kwh) was required to collect and store this solar energy.

Storage - Of the 29.6 million Btu delivered to storage, 19.4 million Btu were subsequently removed for use within the system. Temperature probes within the solar thermal storage tank indicate that the internal energy of the water increased by 1.7 million Btu during the month. This indicates a resulting loss to the environment of 8.5 million Btu through the tank insulation. A further discussion of the tank insulation heat transfer is contained in Section II-D, Observations.

Domestic Hot Water - Domestic hot water is provided to the building by passing city water through a heat exchanger that is immersed in the solar thermal storage tank. A total of 370 gallons of water at an average temperature of 130°F were supplied by this system during March. The average temperature increase was 60°F, which resulted in a measured demand of 0.17 million Btu. All of this energy was supplied by the solar energy system. There was no operating energy required.

<u>Space Heating</u> - Space heating was required during a portion of 18 different days during March. Hot water was pumped from the solar thermal storage tank to a heat exchanger coil in the air ducts to satisfy this requirement. An operating energy expenditure of 0.8 million Btu (229 kwh) was required to satisfy the 5.6 million Btu demand.

<u>Absorption Chiller</u> - The absorption chiller operated on nine occasions to reduce the chilled water storage temperature during March. Use of 0.11 million Btu from the auxiliary conventional cooling system was required to assist the absorption chiller to meet the cooling load on one day of the month. The absorption chiller utilized 13.67 million Btu from the

solar thermal storage tank to remove 7.41 million Btu from the chilled water storage (see attached Auxiliary Performance data). The resulting coefficient of performance of 0.542 compares favorably with the average C.O.P. value of 0.52 observed in this system during the previous five months of operation.

Chilled Water Storage - Performance of the chilled water storage (see attached Auxiliary Storage Performance data) shows that 7.41 million Btu were removed by the chiller, 6.01 million Btu were added from the conditioned space during cooling, and the internal energy of the chilled water storage decreased by 1.45 million Btu. This implies that 0.03 million Btu were lost through the insulation to the environment. Note that the second and third columns of the Auxiliary Storage Performance Table have been changed. The second column, "Energy To Storage", represents the thermal energy removed from the air and put into the chilled water storage tank. The third column, "Energy From Storage", represents the thermal energy removed from the chilled water storage tank by the absorption chiller. In reports prior to February, the values in these columns were reversed. A further discussion of the tank insulation heat transfer is contained in Section II-D, Observations.

Space Cooling - Space cooling was required on all but two of the working days of the month. The space cooling load was 6.17 million Btu. Water from the chilled water storage was pumped through the air duct heat exchangers to remove 6.01 million Btu. Chilled water from the central plant was required to assist in supporting the cooling load during one day of the month - March 5. This resulted from the previous use of the chilled water storage for space cooling, which had raised the storage temperature to a level near the room temperature. Meanwhile, insufficient insolation had prevented use of the absorption chiller.

D. Observations

Previous monthly reports had contained estimates of the insulation performance for the solar thermal and chilled water storage tanks. This

estimate was based on the indicated energy transfer between the tanks and the ambient environment, the monthly average tank and ambient temperatures, and the surface areas of the tanks. However, this estimate has proven not to be accurate when calculated using the monthly averages, particularly when a tank temperature is near the ambient temperature. The transfer of energy through the insulation is an hourly and daily phenomenon and may actually reverse directions during a month duration; the monthly averages do not reflect this information. Additionally, during a period such as this month, when a tank temperature is near ambient, the 0.25° accuracy of the temperature sensors may not be sufficient to quantify the actual temperature differences. These sensors were not intended to be used for this purpose, and the estimate of the insulation performance will be made only when there is sufficient temperature difference to make the sensor errors a small function of the total measurement.

Several of the values in the Storage Performance Table for March may be misleading without additional explanation. As mentioned previously, it is very difficult to make precise energy measurements of the exact amount of energy contained in a large storage tank with three sensors. The occurrence of thermal stratification can become misleading in calculating the average or total energy, and therefore, the value calculated for the change in stored energy may become questionable if the flow into and out of the tank is small. Therefore, the values shown for storage efficiency in the Storage Performance Table may become questionable as the values measured for energy into, energy from, or change in energy of the storage system become quite small (approximately 0.2 million Btu or less).

Near the end of February, all sensors at Reedy Creek were recalibrated to maintain maximum accuracy. Following that recalibration, the temperature sensor for the water exiting the generator of the absorption chiller appears to be indicating a temperature approximately 1.4°F high. Temporary modifications have been incorporated into the performance analysis software to compensate for this, as it is being investigated.

E. Energy Savings

Total system electrical energy savings of 0.9 million Btu (265 kwh) were realized. This value assumes that, had there not been a solar energy system, the energy requirements would have been met by an electrical hot water heater and by a conventional electrical heat pump.

III. ACTION STATUS

The discrepancy of the temperature sensor at the generator exit of the absorption chiller is being investigated.

SOLAR HEATING AND COOLING DEMONSTRATION PROGRAM

MONTHLY REPOR'SITE SUMMARY

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REEDY CREEK PERIOD: MA

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THE LIQUID SYSTEM EMPLOYS 3840 SQ. FT. OF PARABOLIC TROUGH COLLECTORS

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GALLONS OF BOTH HOT AND COLD WATER. AN ABSORPTION CYCLE CHILLER PROVIDES ON THE HOT WATER COIL PROVIDES HEATING AND A COIL SUBMERGED IN THE HOT STORAGE TANK PROVIDES HOT WATER. AUXILLARY COOLING IS PROVIDED BY CHILLED WATER FROM THE CENTRAL COOLING PLANT. THERE IS NO AUXILIARY DHW OR HEATING.

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SOLAR HEATING AND COOLING DEMONSTRATION PROGRAM

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SOLAR HEATING AND COOLING DEMONSTRATION PROGRAM

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MONTHLY REPORT HOT WATER SUBSYSTEM

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SOLAR HEATING AND COOLING DEMONSTRATION PROGRAM

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SOLAR HEATING AND COOLING DEMONSTRATION PROGRAM

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SOLAR HEATING AND COOLING DEMONSTRATION PROGRAM

MONTHLY REPORT AUXILIARY STORAGE PERFORMANCE

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